

Staff Report

Design Review Board

File Number: 7-D-23-DT

Meeting:	7/19/2023
Project:	Hilton Parking Garage
Applicant:	Jerrod Herron Knoxville Properties Partnership

Property Information

Location:500 Clinch Ave.Zoning:DK (Downtown Knoxville)Description:c.1980, concrete parking garage.

Parcel ID 94 L G 00102

Description of Work

Level I Minor Alteration of an Existing Building/Structure, Sign

New signs for parking garage; new flat metal awnings. Awning review is after-the-fact; awnings have already been installed. The awning on Walnut St measures 5' wide and 28' long, and is installed 9.25' above the sidewalk. The awning on Clinch Ave measures 5' wide and 28' long, and is currently installed at 8'-6" above the sidewalk level.

Both signs measure 36" wide by 120" tall (30 sq. ft.), and are internally illuminated, with push-through lights spelling Public Parking. The sign on Walnut St is 11'-6" above the sidewalk, and the sign on Clinch Ave is 10'-10" above the sidewalk. The applicant intends to install the new signs in the same location as the existing projecting signs.

Applicable Design Guidelines

Downtown Design Guidelines

B. Private Realm

1. Building Mass, Scale and Form

1c. Use building materials, cornice lines, signs, and awnings of a human scale in order to reduce the mass of buildings as experienced at the street level.

B. The Traditional Grid District

1. Recommended Signs

1b. Projecting signs of modest size (9 square feet, maximum); a larger sign must be approved by the board.

Comments

The guidelines for the Grid District recommend projecting signs on modest size (9 sq. ft.), with larger signs approved by the Board. New projecting signs approved by the Board are typically around 11-15' sq. ft., with the largest projecting signs approved for businesses on Gay Street. The existing signs were installed prior to the creation of the Downtown Design Review Board and do not conform with the design guidelines. The new signs, both at 30 sq. ft., serve to indicate a parking garage, and should be reduced in size to meet the design guidelines. The internal illumination indicated on the sign drawings meets the guidelines and past Board approvals. The signs should meet the relevant aspects of the City sign code (13.5.B), with its width not extending closer than 20" to the curb.

The awnings were installed without the required City permits and design review approval. Awnings should meet the relevant aspects of the City zoning code, including 10.3.F, which requires a vertical clearance of at least 9' from the sidewalk, not to exceed more than two-thirds width of the sidewalk. The Clinch Avenue awning does not currently meet code as installed, located 8'-6" above the sidewalk, and will need to seek a variance or be removed and reinstalled at least 9' above the sidewalk. Awnings, as installed or revised, should meet the relevant aspects of the City zoning code and building codes.

Recommendation

Staff recommends approval of Certificate 7-D-23-DT, subject to the following conditions: 1) parking signs to be reduced in size, with approval by staff; 2) signs and awnings to meet relevant aspects of City zoning code and building codes, including the necessary revision or after-the-fact approval of awning on Clinch Avenue.





DESIGN REVIEW REQUEST

DOWNTOWN DESIGN (DK)

□ HISTORIC ZONING (H)

□ INFILL HOUSING (IH)

Jerrod	Herron
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Applicant			
6-22-23	July 19, 2023	7-D-23-DT	
Date Filed	Meeting Date (if applicable)	File Number(s)	

CORRESPONDENCE

All correspondence related to this application should be directed to the approved contact listed below.

📕 Owner 🔲 Contractor 🔲 Engine	eer 🗌 Architect/Landscape	Architect		
Jerrod Herron		Knoxville Propert	ies Partnership	
Name		Company		
1225 Weisgarber Rd. Suite 390		Knoxville	TN	37909
Address		City	State	Zip
865-850-3073 jherron@ciprop.com				
Phone	Email			

CURRENT PROPERTY INFO

Knoxville Properties Partnership	1225 Weisgarber Rd		865-850-3073
Owner Name (if different from applicant)	Owner Address		Owner Phone
500 Clinch Ave.		094LG00102	
Property Address		Parcel ID	
		Downtown	
Neighborhood		Zoning	

AUTHORIZATION

Lindsay Crockett	Lindsay Crockett	6.26.23
Staff Signature	Please Print	Date
AL	Jerrod Herron	6-22-23
Applicant Signature	Please Print	Date

REQUEST

DOWNTOWN DESIGN	 Level 1: Signs Alteration of an existing building/structure Level 2: Addition to an existing building/structure Level 3: Construction of new building/structure Site design, parking, See required Downtown Design attachment for more details. Brief description of work: 2 new signs and 2 new awnings on existing 	plazas, landscape ng parking garage		
HISTORIC ZONING	Level 1: Signs Routine repair of siding, windows, roof, or other feature Level 2: Major repair, removal, or replacement of architectural elements or Level 3: Construction of a new primary building Level 4: Relocation of a contributing structure Demolition of a contributing structure Brief description of work:	es, in-kind; Installation materials 🔲 Ad	on of gutters, storm wi	ndows/doors structures
INFILL HOUSING	Level 1: Driveways, parking pads, access point, garages or similar facilities Level 2: Additions visible from the primary street Changes to porches Level 3: New primary structure Site built Modular Multi-Sectional See required Infill Housing attachment for more details. Brief description of work:	Subdivisions	nary street	
STAFF USE ONLY	ATTACHMENTS Downtown Design Checklist Historic Zoning Design Checklist Infill Housing Design Checklist ADDITIONAL REQUIREMENTS Property Owners / Option Holders Level 1: \$50 • Level 2: \$100 • Level 3: \$250 • Level 4: \$500	FEE 1: FEE 2: FEE 3:		TOTAL:











Introduction

This manual provides technical information for Ballew's Products. However, you will often find that a variety of products can work in many applications when you consider span, wind or load—carrying capacity, and design constraints. Ballew's, with support from Britt Peters & Associates can assist in choosing the best system for your specific application. Contact us for help with any of the following:

- System selection
- Product selection
- Building department calculations sealed by a professional engineer
- Shop drawings
- Help with on site application problems

The data contained in this manual is intended to be informative and accurate. However, it is to be used as a technical guideline only and does not replace the judgments and designs of a qualified architect and/or engineer. Ballew's and its engineer do not replace or accept the responsibility of the design professional of record for any structure. However, Ballew's with support from Britt, Peters & Associates, Inc. can provide site specific design and drawings within the following states in which they are registered as Professional Engineers:

Alabama	lowa	New Hampshire	Tennessee
Arizona	Kansas	New Jersey	Texas
Arkansas	Kentucky	New Mexico	Utah
California	Louisiana	New York	Virginia
Colorado	Maryland	North Carolina	Washington
Connecticut	Michigan	Ohio	West Virginia
Florida	Minnesota	Oklahoma	Wisconsin
Georgia	Mississippi	Pennsylvania	Wyoming
Idaho	Missouri	Rhode Island	
Illinois	Nebraska	South Carolina	
Indiana	Nevada	South Dakota	

Neither Ballew's nor Britt, Peters & Associates, Inc. SHALL BE LIABLE FOR INCIDENTAL AND CONSEQUENTIAL DAMAGES, DIRECTLY OR INDIRECTLY SUSTAINED, or for any loss caused by application of these goods for other than the intended use. Ballew's liability is expressly limited to replacement of defective goods.

We reserved the right to change data, table, or charts shown herein without notification.

Ballew's Design Manual

Ballew's Aluminum Products, Inc.

367 Mayfield Road, Duncan, South Carolina 29334 Phone: (864) 272-4453 1-800-231-6666 Fax: (864) 272-4456 Web: www.ballews.com

Britt, Peters and Associates, Inc.

101 Falls Park Drive, Suite 601 Greenville, South Carolina 29601 Phone: (864) 271-8869 Fax: (864) 233-5140 Web: www.brittpeters.com

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2

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Prepared By:

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General Notes

- 1. This Design Manual was Developed in accordance with the "Aluminum Association Specifications For Aluminum Structures, 2005 Edition" and the American Iron And Steel Institute "Cold—Formed Steel Design Manual, 1996 Edition".
- 2. Design criteria utilized in the design of this manual is as follows:

Gravity Loads: Gravity loadings act downward only.

Dead Load: Self weight of canopy members

The maximum snow* or live load is presented in the tables within the manual.

Wind Load: Wind loadings are calculated per ASCE7-05 and the maximum allowable wind speed is reported in the tables within the manual**.

Deflections:

Deck: Span/60

Beams: Span/120

Building Importance Factor: 1.0

Design criteria shall be verified with the local building official.

*The loads presented shall be compared to the flat roof snow load plus the rain on snow surcharge load as defined in ASCE7—05. Where canopies or awnings are adjacent to other structures consult with a professional engineer to evaluate the effects of drift prior to using the tables of this manual.

****** Wind exposure C shall be used unless an exposure B can be verified by a professional engineer. If the structure is located in a flat, unobstructed area or near a large body of water or on an isolated hill consult with a professional engineer prior to using the wind load tables of this manual.

- 3. The material thickness used in design is actual metal thickness. The listed bare metal thickness on all these tables must be the minimum field delivered bare metal thickness.
- 4. It shall be the responsibility of the building permit holder to contact a professional engineer to evaluate the adequacy of existing structures to which the canopy or awning is connected.
- 5. Tabulated information is based on criteria identified here in and precluded to exclusive use of materials supplied by Ballew's Aluminum Products. Consult a professional engineer for special design considerations, local considerations, codes, splice locations, non uniform loading, concentrated loads, snow drifting, partially enclosed situations, web crippling, importance factors other than 1.0, wind exposure factor D, connections to walls, dynamic loading, seismic design, other requirements and additional information not included in this manual.
- 6. Fasteners shall be:
 - a. ¼" and 3/8" diameter bolts shall be 300 series stainless steel or galvanized ASTM A307 bolts;
 - b. 1/2" diameter or greater bolts shall be galvanized ASTM A325 bolts.
 - c. All bolts shall be installed with washer under the bolt heads and nuts.
 - d. All bolt holes shall not be more than 1/16" larger than the bolt diameter.
 - e. #14 stainless steel self tapping screws, hex head, cadmium plated, with 5/8" diameter composite aluminum—neoprene washers (0.05" minimum aluminum thickness)
- 7. Section properties are for information only. Member design is governed by buckling or deflection in many cases and full section capacity may not be developed.
- 8. Dissimilar metals must be separated by painting with bituminous paint or other acceptable coating, or neoprene gasket material to prevent galvanic action.
- 9. Canopies are not designed to be enclosed in any way.
- 10. This manual is for information only. Actual building designs shall be reviewed by a licensed engineer for local conditions, codes, and requirements.

Material Properties

1. The following is a summary of material properties for products specified in this design manual. For further material information refer to Part 4 of the 2005 Aluminum Design Manual and Part 1 of the 2002 AISI Cold—Formed Steel Design Manual.

2.	Alur A	ninum Alloy 3004—H36 Tensile Ultimate Strength
	В.	Tensile Yield Strength $Fty = 28$ KSI
	C.	Compressive Yield StrengthFcy = 25 KSI
	D.	Shear Ultimate StrengthFsu = 20 KSI
	E.	Compressive Modulus of ElasticityE = 10,100 KSI
3.	Alur	ninum Alloy 6005–T5
	A.	Tensile Ultimate StrengthFtu = 38 KSI
	В.	lensile Yield StrengthFty = 35 KSI
	С. р	Compressive field Strength $_{\rm Fcy} = 35$ KSI
	D. F	Shear on induce strength $_{\rm FSU} = 24$ KSI
	L.	compressive modulus of EldsticityL = 10,100 KS
4.	Alur	ninum Alloy 6061–T6
	A. D	Tensile Ultimate Strength $Ftu = 35$ KSI
	Б. С	Compressive Yield Strength Fox = 35 KSI
	D.	Shear Ultimate Strength Fsu = 24 KSI
	E.	Compressive Modulus of ElasticityE = 10,100 KSI
5.	Alur	ninum Alloy 6063–T5
	A.	Tensile Ultimate StrengthFtu = 22 KSI
	В.	Tensile Yield StrengthFty = 16 KSI
	C.	Compressive Yield StrengthFcy = 16 KSI
	D.	Shear Ultimate StrengthFsu = 13 KSI
	E.	Compressive modulus of Elasticity $E = 10,100$ KSI
6.	Alur	ninum Alloy 6063–T6
	A.	Tensile Ultimate StrengthFtu = 30 KSI
	B.	Tensile Yield StrengthFty = 25 KSI
	C.	Compressive Yield Strength Fcy = 25 KSI
	U. E	Snear Ultimate StrengthFsu = 19 KSi Compressive Medulus of ElecticityF = 10 100 KSi
	C.	compressive modulus of Eldsticity = 10,100 KSI
7.	She	et Steel ASTM A1008
	A.	Iensile Ultimate Strength $Fu = 48$ KSI
	в. С	F = 20 KS
	υ.	







19



SECTION VIEW

ISOMETRIC VIEW

SECTION PROPERTIES (COMBINED SECTION):

1.	AREA	0.732	SQUARE INCHES
2.	WEIGHT	0.706	POUNDS PER FOOT
3.	MOMENT OF INERTIA (X-X)	3.7277	IN^4
4.	SECTION MODULUS TOP (X-X)	0.835	IN*3
5.	SECTION MODULUS BOTTOM (X-X)	1.401	IN*3
6.	RADIUS OF GYRATION (X-X)	2.257	IN
7	MOMENT OF INERTIA (Y-Y)	1.0597	104^4
8.	RADIUS OF GYRATION (Y-Y)	1.203	IN
9.	TORSION CONSTANT	7,787	IN^4
10.	POLAR RADIUS OF GYRATION	2.557	IN
NOTES 1.	5: 7" ROLLED GUTTER IS FABRICATED FROM	ALUMINUM	ALLOY 3004-H36.
2.	ROLLED GUTTERS ARE PROVIDED CUT TO	LENGTH.	
3.	TYPICALLY USED TO SUPPORT DECK BET	WEEN COLL	JMNS.
4.	SECTION PROPERTIES ARE FOR INFORMA AND THE FULL SECTION CAPACITY MAY N	TION ONLY OT BE DEVI	. MEMBER DESIGNS ARE OFTEN GOVERNED BY BUCKLING OR DEFLECTION ELOPED.

ITEM NO.	DESCRIPTION	
43-5000	7"x3" Roll Formed Gutter	<i>91.2</i>









UPPER WALL BRACKET CONNECTION DETAIL

DESCRIPTION				FRAME	SIZE			
Marque	Design	Tabl	e	1.5	<u>x1.5'</u>	<u>'x0.1</u> 2	25 " F	Frame
	Projection (Feet)	Spacing (Feet)	Gravity (PSF)	WIND EXP B (MPH)	WIND EXP C (MPH)	Vert. Reaction (LB)	Horiz. Reaction (LB)	
	4.0	1.0	194	150	150	906	2036	
	4.0	2.0	97	150	150	906	2036	1
	4.0	3.0	65	150	150	906	2036	
	4.0	4.0	48	150	130	906	2036	
	4.0	5.0	39	140	110	906	2036	
	4.0	6.0	32	120	100	906	2036	
	4.0	7.0	26	110	90	845	1899	
	5.0	1.0	160	150	150	906	2036	
	5.0	2.0	80	150	150	906	2036	
	5.0	3.0	53	150	130	906	2036	
	5.0	4.0	40	140	110	906	2036	
	5.0	5.0	32	120	100	906	2036	
	5.0	6.0	27	110	90	906	2036	
	5.0	7.0	21	100	85	817	1836	
	6.0	1.0	136	150	150	906	2036	
	6.0	2.0	68	150	150	906	2036	
	6.0	3.0	45	150	120	906	2036	
	6.0	4.0	34	130	100	906	2036	
	6.0	5.0	27	110	90	906	2036	
	6.0	6.0	23	100	85	906	2036	
	7.0	1.0	119	150	150	906	2036	-
	7.0	2.0	59	150	130	906	2036	
	7.0	3.0	40	130	100	906	2036	-
	7.0	4.0	30	110	90	906	2036	_
	7.0	5.0	24	100	-	906	2036	
	8.0	1.0	105	150	140	906	2036	
	8.0	2.0	53	120	100	906	2036	
	8.0	3.0	35	100	85	906	2036	
	8.0	4.0	26	90	-	906	2036	-
	9.0	1.0	94	150	120	906	2036	4
	9.0	2.0	47	100	85	906	2036	4
	9.0	3.0	31	85	-	906	2036	-
	10.0	1.0	85	120	100	906	2036	-
	10.0	2.0	43	90	-	906	2036	

Titen HD® Heavy-Duty Screw Anchor

A high-strength screw anchor for use in cracked and uncracked concrete, as well as uncracked masonry. The Titen HD offers low installation torque and outstanding performance. Designed for use in dry, interior, non-corrosive environments or temporary outdoor applications.

Features

Mechanical Anchors

- Tested in accordance with ACI 355.2, AC193 and AC106
- · Qualified for static and seismic loading conditions
- Thread design undercuts to efficiently transfer the load to the base material
- Standard fractional sizes
- Specialized heat-treating process creates tip hardness for better cutting without compromising the ductility
- No special drill bit required designed to install using standard-sized ANSI tolerance drill bits
- Hex-washer head requires no separate washer, unless required by code, and provides a clean installed appearance
- Removable ideal for temporary anchoring (e.g. formwork, bracing) or applications where fixtures may need to be moved
- · Reuse of the anchor will not achieve listed loads and is not recommended

Codes: ICC-ES ESR-2713 (concrete);

ICC-ES ESR-1056 (masonry); City of LA Supplement within ESR-2713 (concrete); City of LA Supplement within ESR-1056 (masonry); Florida FL15730 (concrete and masonry); FM 3017082, 3035761 and 3043442; Multiple DOT listings

Material: Carbon steel

Coating: Zinc plated or mechanically galvanized.

Not recommended for permanent exterior use or highly corrosive environments.

Installation

- Holes in steel fixtures to be mounted should match the diameter specified in the table below.
 - Use a Titen HD screw anchor one time only installing the anchor multiple times may result in excessive thread wear and reduce load capacity.
- Α
- Do not use impact wrenches to install into hollow CMU. Caution: Oversized holes in base material will reduce or eliminate the
- A mechanical interlock of the threads with the base material and reduce the anchor's load capacity.
- 1. Drill a hole in the base material using a carbide drill bit the same diameter as the nominal diameter of the anchor to be installed. Drill the hole to the specified embedment depth plus minimum hole depth overdrill (see table below) to allow the thread tapping dust to settle, and blow it clean using compressed air. (Overhead installations need not be blown clean.) Alternatively, drill the hole deep enough to accommodate embedment depth and the dust from drilling and tapping.
- 2. Insert the anchor through the fixture and into the hole.
- 3. Tighten the anchor into the base material until the hex-washer head contacts the fixture.

Additional Installation Information

Titen HD [®] Diameter (in.)	Wrench Size (in.)	Recommended Steel Fixture Hole Size (in.)	Minimum Hole Depth Overdrill (in.)
1⁄4	3⁄8	3% to 7⁄16	1⁄8
3⁄8	9⁄16	½ to %16	1⁄4
1/2	3⁄4	5% to 11/16	1/2
5%8	15/16	³ ⁄4 t0 ¹³ ⁄16	1/2
3⁄4	11/8	7⁄8 t0 ¹⁵ ⁄16	1/2

Suggested fixture hole sizes are for structural steel thicker than 12 gauge only. Larger holes are not required for wood or thinner cold-formed steel members.



Cracked

Concrete

Titen HD Screw Anchor

Installation Sequence









Minimum overdrill. See table





Titen HD® Heavy-Duty Screw Anchor

Titen HD Anchor Product Data — Mechanically Galvanized

Size	Model	Thread	Drill Bit	Wrench	Quantity			
(in.)	No.	(in.)	(in.)	(in.)	Вох	Carton		
3% x 3	THD37300HMG	21⁄2			50	200		
3∕8 x 4	THD37400HMG	31⁄2	3/	9/	50	200		
3∕8 x 5	THD37500HMG	41⁄2	78	716	50	100		
3∕8 x 6	THD37600HMG	51⁄2			50	100		
½ x 4	THD50400HMG	31⁄2			20	80		
½ x 5	THD50500HMG	41⁄2			20	80		
½ x 6	THD50600HMG	51⁄2	1/	3/	20	80		
1⁄2 x 6 1⁄2	THD50612HMG	51⁄2	/2	94	20	40		
1⁄2 x 8	THD50800HMG	51⁄2			20	40		
½ x 12	THD501200HMG	51⁄2			5	20		
% x 5	THDB62500HMG	41⁄2			10	40		
5% x 6	THDB62600HMG	51⁄2	5/	15/	10	40		
5∕8 X 6 1⁄2	THDB62612HMG	51⁄2	78	'916	10	40		
5% x 8	THDB62800HMG	51⁄2			10	20		
3∕4 x 5	THD75500HMG	41⁄2			5	20		
3⁄4 x 6	THDT75600HMG	41⁄2	3/	11/	5	20		
3⁄4 X 8 1⁄2	THD75812HMG	51⁄2	94	1 1/8	5	10		
3⁄4 x 10	THD75100HMG	51⁄2			5	10		

C-A-2021 @ 2021 SIMPSON STRONG-TIE COMPANY INC.

SIMPSON

Strong-Tie

IBC S

LW

Mechanical galvanizing meets ASTM B695, Class 65, Type 1. Intended for some pressure-treated wood sill plate applications. Not for use in other corrosive or outdoor environments. See p. 261 or visit strongtie.com/info for more corrosion information.

Titen HD Installation Information and Additional Data¹

Charactaristic	Cumbol	Units	Nominal Anchor Diameter, d _a (in.)										
Gharacteristic	Symbol		1	/4	3,	/8	1	/2	5,	/8		3⁄4	
Installation Information													
Drill Bit Diameter	d _{bit}	in.	1⁄4		3⁄8		1⁄2		5⁄8		3⁄4		
Baseplate Clearance Hole Diameter	d _c	in.	3⁄8		1/2		5⁄8		3⁄4		7⁄8		
Maximum Installation Torque	T _{inst,max}	ftlbf	24 ²		50 ²		65 ²		100 ²		150 ²		
Maximum Impact Wrench Torque Rating	T _{impact,max}	ftlbf	125 ³		150 ³		340 ³		340 ³		385 ³		
Minimum Hole Depth	h _{hole}	in.	1 3⁄4	13/4 25/8		31⁄2	3¾	41⁄2	41⁄2	6	41⁄2	6	6¾
Nominal Embedment Depth	h _{nom}	in.	1%	21⁄2	21⁄2	31⁄4	3¼	4	4	5½	4	5½	6¼
Critical Edge Distance	C _{ac}	in.	3	6	211/16	3%	3%16	41⁄2	41⁄2	6%	6	6%	75⁄16
Minimum Edge Distance	C _{min}	in.	1 1/2						13⁄4				
Minimum Spacing	S _{min}	in.	1 1/2		3					2¾	<i>4</i> 3		
Minimum Concrete Thickness	h _{min}	in.	31⁄4 31⁄2		4	5	5	6¼	6	81⁄2	6	8¾	10
			Ad	ditional [Data								
Anchor Category	Category	—		1									
Yield Strength	f _{ya}	psi	100,000		97,000								
Tensile Strength	f _{uta}	psi	125,000		110,000								
Minimum Tensile and Shear Stress Area	A _{se}	in ²	0.042		0.099		0.183		0.276		0.414		
Axial Stiffness in Service Load Range — Uncracked Concrete	β_{uncr}	lb./in.	202,000		672,000								
Axial Stiffness in Service Load Range — Cracked Concrete	β_{cr}	lb./in.	173	,000	345,000								

1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318-14 Chapter 17 and ACI 318-11 Appendix D.

2. T_{inst,max} is the maximum permitted installation torque for the embedment depth range covered by this table using a torque wrench.

3. Timpact, max is the maximum permitted torque rating for impact wrenches for the embedment depth range covered by this table.

82

Titen HD[®] Design Information — Concrete

Titen HD Tension Strength Design Data¹

Characteristic		Unito	Nominal Anchor Diameter, d _a (in.)										
GildidGteriStic	Бутьог	Units	1/4		3⁄8		1⁄2		5⁄8		3⁄4		
Nominal Embedment Depth	h _{nom}	in.	1% 2½		<mark>2½</mark>	<mark>3¼</mark>	31⁄4	4	4	5½	4	5½	6¼
Steel Strength in Tension — ACI 318-14 Section 17.4.1 or ACI 318-11 Section D.5.1													
Tension Resistance of Steel		lb.	5,1	95	10,890 20, ⁻		,130 30,360		360	45,540			
Strength Reduction Factor — Steel Failure	ϕ_{sa}	—						0.65 ²					
Concrete Breakout Strength in Tension ⁶ — ACI 318-14 Section 17.4.2 or ACI 318-11 Section D.5.2													
Effective Embedment Depth	h _{ef}	in.	1.19	1.94	1.77	<mark>2.40</mark>	2.35	2.99	2.97	4.24	2.94	4.22	4.86
Critical Edge Distance ⁶	C _{ac}	in.	3	6	211/16	211/16 35/8 39/10		41⁄2	41⁄2	6%	6	6%	75⁄16
Effectiveness Factor — Uncracked Concrete		—	30		24 27					24			
Effectiveness Factor — Cracked Concrete		—		17									
Modification Factor	$\Psi_{c,N}$	_	1.0										
Strength Reduction Factor — Concrete Breakout Failure	ϕ_{cb}	—	0.657										
Pullout Strength in Tension — ACI 318-14 Section 17.4.3 or ACI 318-11 Section D.5.3													
Pullout Resistance, Uncracked Concrete (f' $_{\rm c}$ = 2,500 psi)	N _{p,uncr}	lb.	3	<u>3</u>	<mark>2,700</mark> 4	<mark>3</mark>	3	3	3	9,810 ⁴	3	3	3
Pullout Resistance, Cracked Concrete (f'_c = 2,500 psi)	N _{p,cr}	lb.	3	1,9054	<mark>1,235⁴</mark>	2,700 ⁴	3	3	3,0404	5,5704	3	6,070 ⁴	7,1954
Strength Reduction Factor — Concrete Pullout Failure	$\phi_{ ho}$	—	- 0.655										
Tension Strength for Seismic Applications — ACI 318-14 Section 17.4.2.3.3 or ACI 318-11 Section D.3.3.3													
Nominal Pullout Strength for Seismic Loads (f' $_{\rm c}$ = 2,500 psi)	N _{p,eq}	lb.	3	1,9054	<mark>1,235⁴</mark>	2,700 ⁴	3	3	3,0404	5,570 ⁴	3,8404	6,070 ⁴	7,1954
Strength Reduction Factor — Breakout or Pullout Failure		—						0.655					

1. The information presented in this table is to be used in conjunction with the design criteria of ACI 318-14 Chapter 17 and ACI 318-11 Appendix D, except as modified below.

2. The tabulated value of ϕ_{sa} applies when the load combinations of Section 1605.2.1 of the IBC, ACI 318-14 Section 5.3 or ACI 318-11 Section 9.2 are used. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of ϕ_{sa} must be determined in accordance with ACI 318-11 D.4.4. Anchors are considered brittle steel elements.

3. Pullout strength is not reported since concrete breakout controls.

4. Adjust the characteristic pullout resistance for other concrete compressive strengths by multiplying the tabular value by ($f_{c,specified}$ / 2,500)^{0.5}.

5. The tabulated value of ϕ_p or ϕ_{eq} applies when the load combinations of Section 1605.2.1 of the IBC, ACI 318-14 Section 5.3 or ACI 318-11 Section 9.2 are used and the requirements of ACI 318-14 17.3.3.(c) or ACI 318-11 D.4.3(c) for Condition B are met. If the load combinations of ACI 318-11 Appendix C are used, appropriate value of ϕ must be determined in accordance with ACI 318-11 Section D.4.4(c).

6. The modification factor $\Psi_{cp,N} = 1.0$ for cracked concrete. Otherwise, the modification factor for uncracked concrete without supplementary reinforcement to control splitting is either:

)
$$\psi_{cp,N} = 1.0$$
 if $c_{a,min} \ge c_{ac}$ or (2) $\psi_{cp,N} = \frac{c_{a,min}}{c_{cp}} \ge \frac{1.5h_{af}}{c_{cp}}$ if $c_{a,min} < c_{ac}$

The modification factor, $\psi_{cp,N}$ is applied to the nominal concrete breakout strength, N_{cb} or N_{cbg} .

7. The tabulated value of ϕ_{cb} applies when both the load combinations of Section 1605.2.1 of the IBC, ACI 318-14 Section 5.3 or ACI 318-11 Section 9.2 are used and the requirements of ACI 318-14 17.3.3(c) or ACI 318-11 D.4.3(c) for Condition B are met. Condition B applies where supplementary reinforcement is not provided. For installations where complying supplementary reinforcement can be verified, the ϕ_{cb} factors described in ACI 318-14 17.3.3(c) or ACI 318-11 D.4.3(c) for Condition A are allowed. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of ϕ_{cb} must be determined in accordance with ACI 318-11 D.4.4(c).

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